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DESCRIPTION

SWITCHING POWER SUPPLY DEVICE AND ELECTRONIC APPARATUS

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Technical Field

The present invention relates to a switching power supply device and an electronic apparatus including the same.

Background Art

In recent years, the demand for minimizing power consumption during standby when a printing operation is not performed in a printer or a facsimile, for example, has been increasing. Accordingly, a switching power supply device used for a power supply circuit unit of a printer or a facsimile has been required to reduce power consumption in a standby status.

Typically, a switching power supply device of an RCC (rising choke converter) type is used for a power supply circuit unit of those electronic apparatuses. However, the switching power supply device of the RCC type has a characteristic that a switching frequency increases as a load becomes lighter and that switching loss increases accordingly. Under these circumstances, reduction of the power consumption under light load, such as in a standby status, cannot be expected.

Patent Document 1 discloses an example of a switching power supply device of the RCC type capable of reducing power consumption under light load. This switching power supply device includes a circuit to force a control terminal of a first switching element to be grounded for a predetermined time period under light load, so as to delay turn-on of the first switching element and to prevent the switching frequency from exceeding a predetermined value.

However, in the switching power supply device in which the upper limit of the switching frequency is set by the above-described circuit,

a sufficient effect of significantly reducing power consumption by decreasing the switching frequency under light load cannot be obtained.

On the other hand, a switching power supply device for overcoming the above-described problem is disclosed in Patent Document 2. The switching power supply device according to Patent Document 2 includes a circuit for setting a minimum on-period in an on-period of a first switching element so that the minimum on-period is ensured. In this case, the on-period cannot be shortened and thus power is excessively supplied to a load in a standby status, so that an output voltage starts to rise. By providing a circuit for controlling (extending) an off-period upon detecting a slight increase in the output voltage, an increase in the output voltage is prevented and an increase in the switching frequency is suppressed.

Patent Document 1: Japanese Unexamined Patent Application Publication No. 7-67335

Patent Document 2: Japanese Unexamined Patent Application Publication No. 2004-80941

Disclosure of Invention

Problems to be Solved by the Invention

In the switching power supply device according to Patent Document 2, a standby status is detected by detecting that the output voltage has increased. Thus, a difference is caused between a standby output voltage and a rated output voltage. In other words, a variation width of the output voltage is large disadvantageously. Further, two systems of feedback circuits: a feedback circuit for controlling an on-period under non-light load and a feedback circuit for controlling an off-period under light load, are required. Therefore, a gain changes at switching between those systems and also the output voltage changes at switching between the control systems when the load changes.

Accordingly, an object of the present invention is to solve the

above-described two problems by using a single system of a feedback circuit without adopting a method of detecting an increase in output voltage and to provide a switching power supply device in which a variation of the output voltage is suppressed and an electronic apparatus including the same.

Means for Solving the Problems

In order to achieve the above-described object,

(1) a switching power supply device according to the present invention includes: a transformer T including a primary winding N1, a secondary winding N2, and a feedback winding N3; a first switching element Q1 connecting in series to the primary winding N1; a control circuit 4 provided between a control terminal of the first switching element Q1 and the feedback winding N3; a rectifier circuit 2 connecting to the secondary winding N2; and an output voltage control circuit 3 detecting an output voltage output from the rectifier circuit 2 and feeding back the output voltage to the control circuit 4 through one system.

The control circuit 4 includes an on-period control circuit 6 for turning off the first switching element Q1 in an on-state based on a feedback signal transmitted from the output voltage control circuit 3 through one system under non-light load; and an off-period control circuit 5 for controlling an off-period of the first switching element Q1 by delaying turn-on of the first switching element Q1 based on the feedback signal under light load.

(2) In (1), the switching power supply device further includes an impedance circuit 8 provided to connect the off-period control circuit 5 to the on-period control circuit 6, the impedance thereof changing based on the feedback signal. Control of the off-period control circuit 5 under light load and control of the on-period control circuit 6 under non-light load are sequentially performed in

accordance with change in the impedance of the impedance circuit.

(3) In (1) or (2), the off-period control circuit 5 includes a third switching element Q3 provided between the control terminal of the first switching element Q1 and the feedback winding N3 and a fourth switching element Q4 provided between a control terminal of the third switching element Q3 and a ground. The on-period control circuit 6 includes a second switching element Q2 provided between the control terminal of the first switching element Q1 and the ground and a time constant circuit including a capacitor C3 for applying a control voltage to the second switching element Q2. The impedance circuit 8 includes a first path p1 for feeding a current generated by the feedback signal to the capacitor C3 and a second path p2 serving as a bypass for feeding the current to the ground.

(4) In the configuration according to any of (1) to (3), a minimum on-period is set in the on-period controlled by the on-period control circuit 6. Accordingly, the minimum on-period is ensured in every input/output condition, so that intermittent oscillation is prevented.

(5) In (4), the impedance circuit 8 is provided with a clamp circuit for controlling a voltage of the capacitor C3 in the on-period control circuit 6 for determining the control voltage of the second switching element Q2 at a predetermined value when the first switching element Q1 is in an off-state.

(6) In (3), the second path is a bypass circuit for feeding the current generated by the feedback signal only when the first switching element Q1 is in an off-state.

(7) In (1) to (6), the off-period control circuit 5 includes a limit circuit 9 for setting an upper limit of a voltage applied to the control terminal of the first switching element Q1.

(8) An electronic apparatus according to the present invention includes the switching power supply device of any of the above-

described configurations in a power supply circuit unit.

Advantages of the Invention

(1) The on-period control circuit 6 turns off the first switching element Q1 based on the feedback signal from the output voltage control circuit 3 under light load, and the off-period control circuit 5 controls an off-period of the first switching element Q1 by delaying turn on of the first switching element Q1 based on the feedback signal from the output voltage control circuit 3 under non-light load. Accordingly, both on-period and off-period of the first switching element Q1 can be controlled by a feedback circuit of one system. With this configuration, the output voltage does not vary at switching of the control systems when the load changes. Further, since an increase in the output voltage in a standby status need not be detected, no difference occurs between the output voltage in a standby status and the output voltage in a rated status, so that a variation width of the output voltage does not become large.

(2) The impedance of the impedance circuit connecting the off-period control circuit 5 and the on-period control circuit 6 changes based on the feedback signal from the output voltage control circuit 3, and based the change, control of the off-period control circuit 5 under light load and control of the on-period control circuit 6 under non-light load are sequentially performed. Accordingly, an increase in ripple or a variation in the output voltage does not occur at the switching between on-period control and off-period control.

(3) The impedance circuit includes the first path p1 for feeding a current generated by the feedback signal to the capacitor C3 of the on-period control circuit 6 and the second path p2 that extends to the ground while bypassing the on-period control circuit 6. With this configuration, by changing the rate of the current to be fed to the ground through the bypass, an on-period under light load can be set.

Accordingly, a relationship between a power supplied to the load and the switching frequency (frequency characteristic) can be set.

(4) By setting the minimum on-period in the on-period controlled by the on-period control circuit 6, the minimum on-period can be ensured in every input/output condition, so that intermittent oscillation can be prevented even under no load.

(5) When the first switching element Q1 is in an off-state, the clamp circuit controls the voltage of the capacitor determining the control voltage of the second switching element Q2 at a constant voltage and extends the off-period without limit. Accordingly, an increase in the output voltage under no load can be prevented.

(6) When the first switching element Q1 is in an off-state, the bypass circuit allows the current generated by the feedback to detour so that the charging amount in an on-period and the charging amount in an off-period of the capacitor C3 can be independently changed. Accordingly, the degree of freedom of setting the relationship between a power supplied to the load and the switching frequency (frequency characteristic) can be further increased.

(7) The limit circuit sets the upper limit of the voltage applied to the control terminal of the first switching element Q1, which enables the use over a wide input voltage range.

(8) According to the electronic apparatus of the present invention, a constantly stable operation can be realized because the power supply voltage to the load varies only slightly regardless of the status of the load.

Brief Description of the Drawings

[Fig. 1] Fig. 1 is a circuit diagram of a switching power supply device according to a first embodiment.

[Fig. 2] Fig. 2 shows voltage waveforms of respective components in the switching power supply device.

[Fig. 3] Fig. 3 is a circuit diagram of a switching power supply device according to a second embodiment.

[Fig. 4] Fig. 4 shows voltage waveforms of respective components in the switching power supply device.

[Fig. 5] Fig. 5 is a circuit diagram of a switching power supply device according to a third embodiment.

[Fig. 6] Fig. 6 is a circuit diagram of a switching power supply device according to a fourth embodiment.

[Fig. 7] Fig. 7 is a block diagram showing a configuration of a printer according to a fifth embodiment.

Reference Numerals

1	switching power supply device
2	rectifier circuit
3	output voltage control circuit
4	control circuit
5	off-period control circuit
6	on-period control circuit
7	negative feedback circuit
8	impedance circuit
9	limit circuit
p1	first path
p2	second path
T	transformer
N1	primary winding
N2	secondary winding
N3	feedback winding
Vcc	DC power supply
Q1	first switching element
Gin	input-power-supply-side ground
SR	shunt regulator

Best Mode for Carrying Out the Invention

<First Embodiment>

A switching power supply device according to a first embodiment is described with reference to Figs. 1 and 2.

Fig. 1 is a circuit diagram of the switching power supply device. This switching power supply device includes a transformer T including a primary winding N1, a secondary winding N2, and a feedback winding N3; a first switching element Q1 connecting in series to the primary winding N1; a control circuit 4 provided between a control terminal of the first switching element Q1 and the feedback winding N3; a rectifier circuit 2 connecting to the secondary winding N2; and an output voltage control circuit 3 for detecting an output voltage output from the rectifier circuit 2 and feeding it back to the control circuit 4. The first switching element Q1 includes a MOSFET and applies a DC power Vcc as an input power to a series circuit composed of the first switching element Q1 and the primary winding N1.

The rectifier circuit 2 includes a diode D1 connecting in series to the secondary winding N2 and a smoothing capacitor C1 connecting between a cathode of the diode D1 and a ground. A secondary-side circuit including the secondary winding N2, the diode D1, and the capacitor C1 and a primary-side circuit in which the first switching element Q1 is provided in series constitute a main circuit.

The output voltage control circuit 3 includes a voltage dividing circuit composed of resistors R2 and R3 between an output terminal Po and a ground Gout and also includes a series circuit composed of a resistor R1, a photodiode PD1 of a photocoupler PC1, and a shunt regulator SR. Further, the output voltage control circuit 3 includes a negative feedback circuit 7 composed of a series circuit of a resistor R15 and a capacitor C9 between a node of the resistors R2 and R3 and a cathode terminal of the shunt regulator SR. Additionally,

the node of the resistors R2 and R3 connects to a reference terminal of the shunt regulator SR.

The control circuit 4 includes an off-period control circuit 5 and an on-period control circuit 6. A third switching element Q3 and a capacitor C2 of the off-period control circuit 5 are provided in series between one end of the negative feedback winding N3 and a gate of the first switching element Q1. A series circuit composed of a resistor R13 and a capacitor C10 of the off-period control circuit 5 constitutes a time constant circuit. A series circuit composed of a resistor R9 and a fourth switching element Q4 connects between a base of the third switching element Q3 and an input-power-supply-side ground Gin. Resistors R23 and R24 connect between a base of the fourth switching element Q4 and the capacitor C10. A resistor R22 and a capacitor C11 are provided between the base of the fourth switching element Q4 and the input-power-supply-side ground Gin. A capacitor C6 for preventing a malfunction caused by noise is provided between the base and emitter of the third switching element Q3. A resistor R4 for startup connects between a terminal on the first switching element Q1 side of the capacitor C2 and an input power supply line.

A series circuit composed of a phototransistor PT1 of the photocoupler PC1 and a resistor R16 is provided between a node of the resistors R23 and R24 and the input-power-supply-side ground Gin.

A second switching element Q2 is provided between the gate of the first switching element Q1 and the input-power-supply-side ground Gin in the on-period control circuit 6. A time constant circuit composed of the resistors R6 and R7 and the capacitor C3 is provided across the feedback winding N3. One terminal of the capacitor C3 connects to the base of the second switching element Q2 so that the voltage of the capacitor C3 is applied between the base and emitter of the second switching element Q2.

A diode D4 connects between a node of the phototransistor PT1 and

the resistor R16 and the base of the second switching element Q2. A gate protecting resistor R21 connects between the gate and source (Gin) of the first switching element Q1.

The above-described phototransistor PT1, the resistors R16 and R24, and the diode D4 constitute an impedance circuit 8. The impedance of the phototransistor PT1 is changed by a feedback signal transmitted through the photodiode PD1.

A first feature of the switching power supply device shown in Fig. 1 is that the circuitry is configured so as to feed a current of the phototransistor PT1 through the diode 4 to the capacitor C3 (for charging) and also to feed the current through the resistor R16 to the input-power-supply-side ground Gin (through a bypass).

A second feature is that the circuitry is configured so as to control an on-timing of the fourth switching element Q4 by using the impedance circuit 8 and a time constant circuit composed of the resistors R22 and R23 and the capacitor C11.

An operation of the switching power supply device shown in Fig. 1 is as follows.

<1.1> Under light load

An off-period of the first switching element Q1 is controlled to keep an output voltage constant under light load, as described below.

<1.1.1> Off-period of the first switching element Q1

(Operation of the main circuit)

In an off-period of the first switching element Q1, an exciting energy of the transformer T (the energy accumulated during an on-period of the first switching element Q1) is output to the secondary side. In a typical RCC, when an exciting current (herein, a current flowing through the secondary winding N2) becomes 0 (zero), a resonance voltage is generated in the feedback winding N3 and the first switching element Q1 is turned on and shifts to an on-period. In the circuit shown in Fig. 1, however, the first switching element

Q1 cannot be turned on until the third switching element Q3 is turned on. Therefore, turn-on of the third switching element Q3 is a necessary condition to end an off-period of the first switching element Q1 under light load. By turning on the third switching element Q3, the first switching element Q1 is turned on by a charge accumulated in the capacitor C2 and shifts to an on-period.

(Operation of the control circuit)

The impedance of the phototransistor PT1 determines a time period until the fourth switching element Q4 is turned on. That is, since a large current flows through the photodiode PD1 of the photocoupler PC1 under light load, the impedance of the phototransistor PT1 decreases and a voltage of a collector terminal of the phototransistor PT1 also decreases. Since the base-emitter voltage of the fourth switching element Q4 (the voltage of the capacitor C11) depends on the time constant circuit composed of the resistors R22 and R23 and the capacitor C11, the time period until the fourth switching element Q4 is turned on depends on the voltage of the collector terminal of the phototransistor PT1. Therefore, an off-period of the first switching element Q1 becomes longer as the collector voltage of the phototransistor PT1 is lower under light load. This is an operation of a current discontinuous mode.

<1.1.2> On-period of the first switching element Q1

(Operation of the main circuit)

After the first switching element Q1 is turned on, a current flows through a path: Vcc → the primary winding N1 of the transformer T → Q1 → Gin, so that energy is accumulated in the transformer T. When the second switching element Q2 is turned on, the first switching element Q1 is turned off and shifts to an off-period.

(Operation of the control circuit)

During an on-period of the first switching element Q1, the capacitor C3 is charged by a voltage generated in the feedback winding

N3. At this time, the voltage of the feedback winding N3 causes a current to flow to the time constant circuit composed of the resistors R6 and R7 and the capacitor C3, so that the charging voltage of the capacitor C3 rises. Further, a voltage of the capacitor C10 causes a current to flow to a parallel circuit composed of the capacitor C3 and the resistor R7 through a first path p1 including the phototransistor PT1 and the diode D4, so that the charging voltage of the capacitor C3 rises.

When the voltage of the capacitor C3 reaches an on-voltage Vbe(on) of the second switching element Q2, the second switching element Q2 is turned on and an off-period of the first switching element Q1 starts.

Under light load, the voltage of the capacitor C3 at the time when the first switching element Q1 is turned on is relatively high. This is because the impedance of the phototransistor PT1 is low and a large amount of charge is accumulated in the capacitor C3 during an off-period of the first switching element Q1. Therefore, the voltage of the capacitor C3 reaches Vbe(on) of the second switching element Q2 in a short on-period of the first switching element Q1. Then, turn-on of the second switching element Q2 causes turn-off of the first switching element Q1.

<1.2> Under heavy load

Under heavy load or non-light load, the output voltage is kept constant by controlling an on-period of the first switching element Q1 as in a typical RCC, as described below.

<1.2.1> Off-period of the first switching element Q1

(Operation of the main circuit)

In an off-period of the first switching element Q1, the exciting energy of the transformer T is output to the secondary side. When the exciting current of the transformer T becomes 0 (zero), a resonance voltage is generated in the feedback winding N3. At this time, the third switching element Q3 is in an on-state, and thus the first

switching element Q1 is turned on by the resonance voltage and shifts to an on-period.

(Operation of the control circuit)

Under heavy load, since a current of the photodiode PD1 of the photocoupler PC1 is small, the impedance of the phototransistor PT1 is high and the collector voltage of the phototransistor PT1 is also high. Accordingly, a charging time of the capacitor C11 is short and a turn-on timing of the fourth switching element Q4 comes early. For this reason, the time constant is set so that the fourth switching element Q4 is already turned on when the exciting current of the transformer T reaches 0 (zero) under heavy load. Thus, the third switching element Q3 is in an on-state, and the first switching element Q1 is turned on immediately after a resonance voltage is generated in the feedback winding N3. This is an operation of a current critical mode like a typical RCC.

Since the impedance of the phototransistor PT1 is high, a small current flows from the capacitor C10 through a path: PT1 → D4 → (C3+R7), so that a small amount of charge is accumulated in the capacitor C3. Further, since the capacitor C3 is negatively charged due to the voltage of the feedback winding N3, the first switching element Q1 shifts to an on-period such that the capacitor C3 is in a negative potential.

<1.2.2> On-period of the first switching element Q1

(Operation of the main circuit)

After the first switching element Q1 is turned on, a current flows through a path: Vcc → N1 → Q1 → Gin, so that energy is accumulated in the transformer T. Turn-on of the second switching element Q2 causes turn-off of the first switching element Q1. That is, the first switching element Q1 shifts to an off-period.

(Operation of the control circuit)

During an on-period of the first switching element Q1, a current

flows to a parallel circuit composed of the capacitor C3 and the resistor R7 through the resistor R6 by a voltage generated in the feedback winding N3. Also, a voltage of the capacitor C10 causes a current to flow through a path: PT1 → D4 → (C3+R7), so that the capacitor C3 becomes charged. At first, the capacitor C3 is in a negative potential. However, when the potential of the capacitor C3 reaches the on-voltage Vbe(on) of the second switching element Q2 by the charge, the first switching element Q1 is turned off and shifts to an off-period. In other words, the impedance of the phototransistor PT1 causes a change in an on-period of the first switching element Q1, so that a constant voltage control is performed.

Fig. 2 shows voltage waveforms of respective components shown in Fig. 1 under light load and heavy load. Herein, (A) shows a light load status and (B) shows a heavy load status. In the figure, V(C11) indicates the voltage of the capacitor C11, V(C3) indicates the voltage of the capacitor C3, Q4Vbe(On) indicates a base-emitter threshold voltage required by the fourth switching element Q4 to be turned on, and Q2Vbe(On) indicates a base-emitter threshold voltage required by the second switching element Q2 to be turned on.

Under light load, as shown in (A), the second switching element Q2 is turned on when the voltage V(C3) reaches Q2Vbe(On) at the timing of "to" and the first switching element Q1 is turned off accordingly. The turn-off of the first switching element Q1 causes a reverse voltage (flyback voltage) to be generated in the feedback winding N3 and the collector potential of the second switching element Q2 turns to a negative potential. Accordingly, a current reversely flows between the base and collector of the second switching element Q2, so that the capacitor C3 is discharged quickly.

After that, a reverse voltage generated in the feedback winding N3 causes the capacitor C3 to be negatively charged through a path: C3 → R6 → N3 during a period from "to" to "t1". Also, the capacitor C11 is

discharged (negatively charged) through a path: C11 → base-collector of Q4 → R9 → C6 → N3. Although the capacitor C11 has been charged through a path: C10 → R24 → R23 → C11, the impedance of the phototransistor PT1 is low under light load and its effect is small.

At the timing of "t1" when the voltage of the feedback winding N3 turns from negative to positive and when the energizing current of the transformer T becomes 0 (zero), the capacitor C11 is charged through a path: C10 → R24 → R23 → C11. At this time, a current also flows through a path: R24 → PT1 → R16, and thus the charging time constant of the capacitor C11 changes in accordance with the impedance of the phototransistor PT1. In other words, a rising inclination denoted by "A" in the figure of V(C11) from "t1" to "t2" changes depending on the load.

For example, since the impedance of the phototransistor PT1 becomes smaller as the load becomes lighter, the charging time constant of the capacitor C11 increases and a degree of the inclination A decreases. Conversely, the impedance of the phototransistor PT1 becomes higher as the load becomes heavier, and thus the charging time constant of the capacitor C11 decreases and a degree of the inclination A increases. Accordingly, the on-timing of the fourth switching element Q4 changes and the on-timing of the third switching element Q3, that is, the on-timing of the first switching element Q1 changes. As a result, the off-period of the first switching element Q1 is controlled and a constant voltage is output. At this time, the capacitor C3 is charged through a path: C10 → R24 → PT1 → D4 → C3, so that the voltage V(C3) rises.

When the first switching element Q1 is turned on at time "t2", the capacitor C3 is charged through a path: N3 → R6 → C3. As can be seen in the figure, the voltage V(C3) rises in the period from "t2" to "to" more sharply than in the period from "t1" to "t2". When the voltage V(C3) reaches Q2Vbe(On) at time "to", the second switching element Q2

is turned on and the first switching element Q1 is turned off.

Under heavy load, as shown in (B), the second switching element Q2 is turned on when the voltage V(C3) reaches Q2Vbe(On) at the timing of "to" and the first switching element Q1 is turned off accordingly. The turn-off of the first switching element Q1 causes a reverse voltage (flyback voltage) to be generated in the feedback winding N3 and the collector potential of the second switching element Q2 turns to a negative potential. Accordingly, a current reversely flows between the base and collector of the second switching element Q2, so that the capacitor C3 is discharged quickly.

After that, a reverse voltage generated in the feedback winding N3 causes the capacitor C3 to be negatively charged through a path: C3 → R6 → N3 during the period from "to" to "t1". Since a positive charging path C10 → R24 → PT1 → D4 → C3 also exists, the negative charging time constant of the capacitor C3 depends on the impedance of the phototransistor PT1. Under heavy load, the impedance of the phototransistor PT1 is relatively high and thus the collector voltage of the phototransistor PT1 is also high. Therefore, the capacitor C11 is hardly discharged and is quickly charged in the period from "t0" to "t1", and the fourth switching element Q4 is already turned on at time "t1". Thus, the third switching element Q3 is also turned on.

As described above, since the fourth switching element Q4 is already in an on-state at the timing "t1", the first switching element Q1 is turned on based on the resonance voltage of the feedback winding N3 thereafter.

Then, the capacitor C3 is positively charged through a path: N3 → R6 → C3. Then, when the voltage V(C3) reaches Q2Vbe(On) at the timing "to", the second switching element Q2 is turned on and the first switching element Q1 is turned off.

Under heavy load, as shown in (B) of Fig. 2, the on-period of the first switching element Q1 ("t1" to "to") changes in accordance with a

change in the inclination denoted by B in the figure of the voltage V(C3) of the capacitor C3 due to the load. For example, since the impedance of the phototransistor PT1 becomes lower as the load becomes lighter, the charging time constant in a positive direction to the capacitor C3 through the first path p1 becomes small, the inclination B becomes gradual, and the voltage V(C3) at the turn-on timing of the first switching element Q1 becomes higher as indicated by "Po2". As a result, the voltage V(C3) reaches Q2Vbe(On) more quickly and thus the on-period of the first switching element Q1 becomes shorter. Conversely, since the impedance of the phototransistor PT1 becomes higher as the load becomes heavier, the charging time constant in a positive direction to the capacitor C3 through the first path p1 becomes large, the inclination B becomes sharp, and the voltage V(C3) at the turn-on timing of the first switching element Q1 becomes lower as indicated by "Po1". As a result, the voltage V(C3) reaches Q2Vbe(On) more slowly and thus the on-period of the first switching element Q1 becomes longer.

In this way, the on-period of the first switching element Q1 is controlled in accordance with the load, so that a constant voltage is output.

Since the negative feedback circuit 7 is provided in the output voltage control circuit 3, a current flowing to the photodiode PD1 of the photocoupler PC1 does not decrease abruptly and the phototransistor PT1 constantly operates in an active region. Therefore, the photodiode PD1 is not turned on/off depending on a voltage variation (output ripple) of the output terminal Po, and the switching frequency is determined by the constant of a CR in the off-period control circuit 5 and the on-period control circuit 6.

As described above, operation modes under light load (standby status) and under heavy load (rated status) are not switched by an increase in the output voltage, and thus no difference arises between

the output voltage in a standby status and the output voltage in a rated status. Furthermore, the use of the single-circuit feedback system can prevent an inconvenience of a variation in the output voltage, which is caused by a change in gain due to switching between two circuits of feedback systems for the on-period control circuit 6 and the off-period control circuit 5.

<Second Embodiment>

Next, a switching power supply device according to a second embodiment is described with reference to Figs. 3 and 4.

Fig. 3 is a circuit diagram of the switching power supply device. Unlike in the switching power supply device shown in Fig. 1 according to the first embodiment, a diode D3 connects in series to the resistor R16. The other configuration is the same as that shown in Fig. 1.

In the first embodiment, the capacitor C3 is positively charged through a path: C10 → R24 → PT1 → D4 → C3 in an off-period of the first switching element Q1. Under no load, however, the impedance of the phototransistor PT1 becomes a minimum and the potential of the capacitor C3 sharply increases, and thus the second switching element Q2 can be turned on before the third switching element Q3 is turned on according to setting of a circuit constant. In that case, even after the third switching element Q3 is turned on, no voltage is applied to the gate of the first switching element Q1 and the first switching element Q1 cannot be turned on. This causes an intermittent oscillation status. In the intermittent oscillation status, an oscillation period is long, so that the following capability at a sudden change in load degrades.

In the second embodiment, the diode D3 connects in series to the resistor R16 as described below. With this configuration, the voltage of the capacitor C3 can be clamped to a constant voltage in an off-period of the first switching element Q1. Further, by setting this voltage at low so that the second switching element Q2 cannot be

turned on, turn-on of the second switching element Q2 in an off-period of the first switching element Q1 can be prevented, and thus intermittent oscillation can be prevented.

An operation of the switching power supply device shown in Fig. 3 (the operation different from that of the switching power supply device shown in Fig. 1) is as follows.

<2.1> Under light load

Under light load, an on-period of the first switching element Q1 is fixed and the output voltage is kept constant by controlling an off-period of the first switching element Q1.

<2.1.1> Off-period of the first switching element Q1

(Operation of the main circuit)

The same as in the first embodiment. That is, under light load, turn-on of the third switching element Q3 is a necessary condition to end an off-period of the first switching element Q1. The first switching element Q1 shifts to an on-period upon turn-on of the third switching element Q3.

(Operation of the control circuit)

A current flowing through the phototransistor PT1 is divided into a current flowing through a path p2 including the resistor R16 and the diode D3 and a current flowing through a path p1 for charging the capacitor C3 through the diode D4. The capacitor C3 is charged by the current flowing through the path p1 including the diode D4, but the voltage V(C3) thereof is clamped to a constant voltage by the diodes D3 and D4 and the resistor R16. Herein, assuming that a forward dropping voltage of the diode D3 is VF(D3), that a dropping voltage of the resistor R16 is VR16, and that a forward dropping voltage of the diode D4 is VF(D4), the emitter terminal voltage of the phototransistor PT1 is clamed to VF(D3)+VR16, and thus a clamp voltage V(C3)CL of the capacitor C3 can be represented by the following expression:

V(C3)CL=VF(D3)+VR16-VF(D4).

<2.1.2> On-period of the first switching element Q1

(Operation of the main circuit)

As in the first embodiment, a current flows through a path: Vcc → N1 → Q1 → Gin and energy is accumulated in the transformer T. When the second switching element Q2 is turned on, the first switching element Q1 is turned off and shifts to an off-period.

(Operation of the control circuit)

Under light load, an on-period is fixed.

That is, at the time when the first switching element Q1 is turned on, a base voltage of the second switching element Q2 (the voltage V(C3) of the capacitor C3) is kept at the above-described clamp voltage: V(C3)=VF(D3)+VR16-VF(D4), and then the capacitor C3 is charged by a voltage generated in the feedback winding N3. The time constant at this time is determined by the circuit composed of the resistors R6 and R7 and the capacitor C3 regardless of the impedance of the phototransistor PT1 and so on. As described above, since the initial value of the charge in the capacitor C3 and the time constant of the time constant circuit composed of the resistors R6 and R7 and the capacitor C3 are constant, the on-period is fixed. When the voltage of the capacitor C3 reaches the on-voltage Vbe(On) of the second switching element Q2, the second switching element Q2 is turned on and the first switching element Q1 shifts to an off-period.

<2.2> Under heavy load

Under heavy load, the same operation as that in the first embodiment is performed.

Fig. 4 shows voltage waveforms of respective components shown in Fig. 1 under light load and under heavy load. (A) shows a light load status and (B) shows a heavy load status. Under light load, as shown in (A), the voltage V(C3) of the capacitor C3 is clamped to a constant voltage by the diodes D3 and D4 and the resistor R16 during an off-

period of the first switching element Q1. Therefore, the initial value of the charge in the capacitor C3 is constant as indicated by a point A1. Further, since the time constant of the time constant circuit composed of the resistors R6 and R7 and the capacitor C3 is constant, an on-period of the first switching element Q1 is fixed.

As described above, by clamping the voltage of the capacitor C3 to a constant value, the voltage V(C3) does not reach Q2Vbe(On) during an off-period of the first switching element Q1 even under no load and the second switching element Q2 is not turned on. Accordingly, a minimum on-period of the first switching element Q1 is set and intermittent oscillation can be prevented.

<Third Embodiment>

Next, a switching power supply device according to a third embodiment is described with reference to Fig. 5.

Fig. 5 is a circuit diagram of the switching power supply device. This switching power supply device is different from that shown in Fig. 3 in that a switching element Q5, resistors R17, R18, R19, and R20, and a diode D5 are added. These added components operate in the following manner.

(a) The diode D5 and the resistors R17 to R20 detect on/off of the fourth switching element Q4 to control on/off of the switching element Q5. That is, turn-on of the fourth switching element Q4 causes a current to flow through a path: R20 → R19 → D5 → Q4. Accordingly, the potential at a node between the resistors R20 and R19 decreases and a base potential of the switching element Q5 decreases, so that the switching element Q5 is turned off. On the other hand, turn-off of the fourth switching element Q4 causes the base potential of the switching element Q5 to rise, which turns on the switching element Q5.

(b) During an off-period of the first switching element Q1 (during an off-period of the fourth switching element Q4), the diodes D3 and D4, the resistor R16, and the switching element Q5 feed a current of

the phototransistor PT1 to the input-power-supply-side ground Gin through the diode D3 and the resistor R16 by turn-on of the switching element Q5. On the other hand, during an on-period of the first switching element Q1 (during an on-period of the fourth switching element Q4), the capacitor C3 is charged with the current of the phototransistor PT1 through the diode D4 by turn-off of the switching element Q5.

The operation of the other circuits is the same as in the first and second embodiments.

As described above, the amount of electric charge to be applied to the capacitor C3 during an on-period of the first switching element Q1 can be changed without depending on the path of the resistor R16, so that the degree of freedom of setting can be increased.

For example, assume that the resistor R16 in the circuits shown in Figs. 1 and 3 according to the first and second embodiments is a low-resistance resistor. In this case, most part of the current flowing through the phototransistor PT1 flows through a path including the diode D3 and the resistor R16, so that the voltage of the capacitor C3 gradually rises during an on-period of the first switching element Q1. In this case, intermittent oscillation may occur due to a too long on-period under light load or no load. At the worst, the output voltage rises. This problem is well managed in the second embodiment compared to in the first embodiment, but the problem occurs in some specifications. On the other hand, in the third embodiment, the path including the diode D3 and the resistor R16 is interrupted by the switching element Q5 in an on-period of the first switching element Q1, and thus the above-described problem does not occur.

<Fourth Embodiment>

Next, a switching power supply device according to a fourth embodiment is described with reference to Fig. 6.

Fig. 6 is a circuit diagram of the switching power supply device.

This switching power supply device is different from that shown in Fig. 3 according to the second embodiment in that the circuit composed of the switching element Q3, the capacitor C6, and the resistor R9 shown in Fig. 3 is replaced by a voltage regulator circuit composed of resistors R25, R26, and R27, switching elements Q8 and Q9, and a Zener diode D8.

Herein, the switching element Q8 and the Zener diode D8 constitute the voltage regulator circuit, whereas the switching element Q9 and the resistors R25 and R26 constitute an inverting circuit for inverting a voltage signal.

This switching power supply device has the following advantage in addition to that of the switching power supply device shown in Fig. 3 according to the second embodiment.

The Zener diode D8 constitutes a constant voltage regulator (limit circuit) together with the switching element Q8 and limits the gate voltage (control voltage) of the first switching element Q1 so that the gate voltage does not exceed a predetermined range. That is, the gate voltage of the first switching element Q1 is controlled not to exceed a maximum: $Vgs(Q1)=Vz(D8)-Vbe(Q8)$.

Herein, $Vgs(Q1)$ is a gate-source voltage of the first switching element Q1, $Vz(D8)$ is a Zener voltage of the Zener diode D8, and $Vbe(Q8)$ is a forward base-emitter voltage of the switching element Q8.

With this configuration, the control voltage of the first switching element Q1 can be prevented from exceeding the predetermined voltage over a wide input voltage range, such as a World Wide input, and thus the first switching element Q1 can be protected from breakdown.

<Fifth Embodiment>

Next, an electronic apparatus according to a fifth embodiment is described with reference to Fig. 7. Fig. 7 is a block diagram showing a configuration of a printer. A rectifier circuit 10 receives a power

supply voltage of a commercial AC power supply AC, rectifies the power supply voltage, and outputs the power supply voltage to a switching power supply device 1. This switching power supply device 1 corresponds to the switching power supply device according to any of the first to fourth embodiments. A printer control circuit 11 operates by using a DC power supply voltage output from the switching power supply device 1 as power. The printer control circuit 11 transmits/receives data to/from a host apparatus through a communication unit 12 and a communication line, reads an operation of an operation unit 13, and drives a drive unit 14.

The drive unit 14 consumes power during a printing operation but hardly consumes power during a standby status when no printing operation is performed. Since the switching power supply device 1 of the present invention is used, power loss in a standby status can be reduced and the efficiency can be increased.

The electronic apparatus of the present invention is not limited to the printer, but various electronic apparatuses requiring a DC power supply of a stable voltage, such as a notebook personal computer and a portable information apparatus, can also be applied.